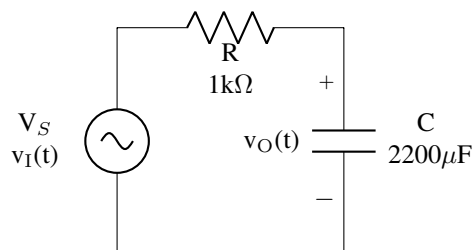


CHAPTER 14

FOURIER SERIES AND CIRCUIT ANALYSIS

Estimate $v_O(t)$ using the complex Fourier series ($k=0..100$), the function $v_I(t) = \sin\left(\frac{4\pi}{3}t\right) [u(t+3) - u(t-0)]$ on the interval $-4 \leq t \leq 4$, and the circuit below:



```
1 clear all
2 close all
3 clc
4 format short eng
5
6 syms x w t T integrand
7
8 n=100; %# of coefficients to find
9 T0=8; %Frequency of the cosine
10 w0=(2*pi)/T0; % period that corresponds to w0
11 x=@(t) sin((4*pi/3).*t).*(heaviside(t+3)-heaviside(t));
12 t0=-4; t1=4;
13
14 tk=t0:T0/1000:t1;
15 figure(1)
16 plot(tk,x(tk),'LineWidth',3)
17
18 for k=0:n;
```

```

19     integrand=@(t) (x(t)).*cos(k.*w0.*t);
20     a(k+1)=(2/T0)*integral(integrand,t0,t1);
21
22     integrand=@(t) (x(t)).*sin(k.*w0.*t);
23     b(k+1)=(2/T0)*integral(integrand,t0,t1);
24 end
25
26 figure(2)
27 hold on;grid on
28 plot(0:length(a)-1,a,'x','LineWidth',4,'MarkerSize',10)
29 plot(0:length(a)-1,b,'ro','LineWidth',4,'MarkerSize',10)
30
31 xlabel('Multiple of the fundamental frequency - k')
32 ylabel('Coefficient')
33 legend('a_k','b_k')
34
35 x_hat=(a(1)/2);
36 for k=1:n;
37     x_hat=x_hat+ a(k+1).*cos(k.*w0.*tk)+ b(k+1).*sin(k.*w0.*tk);
38 end
39 set(findall(gcf,'-property','FontSize'),'FontSize',14)
40
41 figure(3)
42 hold on;grid on
43 plot(tk,x(tk),'ro')
44 plot(tk,x_hat,'LineWidth',3)
45
46 %perform ckt analysis
47 syms s
48 Hs=1/(2.2*s+1)
49
50 %DC component output
51 vo_hat=(a(0+1)/2)*(1); %DC input times DC gain
52
53 for k=1:n
54     H=subs(Hs,s,j*k*w0); % Find gain at multiple of w0
55     Vi=a(k+1)-j*b(k+1);
56     Vo=Vi*H;
57     vo_hat=vo_hat+eval(abs(Vo)).*cos(k.*w0.*tk+eval(angle(Vo)));
58 end
59
60 plot(tk,vo_hat,'g','LineWidth',3)
61 xlabel('Time (s)')
62 legend('x(t)','x_hat(t)')
63 set(findall(gcf,'-property','FontSize'),'FontSize',14)

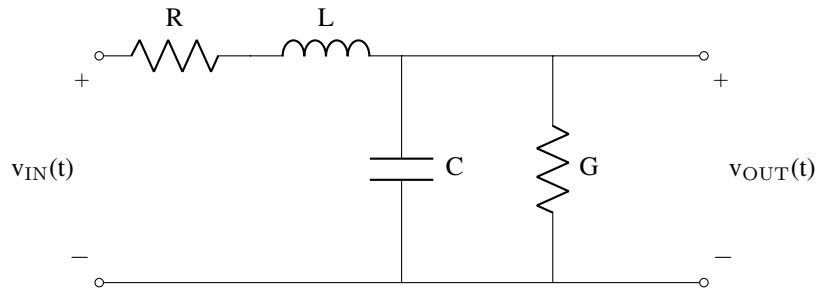
```

14.1 Application to Data Transmission

Let's revisit an example from an earlier chapter. We looked at the frequency response of a transmission line when we were first developing transfer functions and Bode plots. Now we have the tools necessary to send a signal down that transmission line and determine what comes out the other end.

■ EXAMPLE 14.1

Here is the transmission line model we studied earlier



I'll include the parameters again for completeness. I'll also include the values we used for two lengths of cable and I will add a third. The third length we'll consider is 3280 ft (1000 m), far longer than the limit for an ethernet cable. Often when I'm trying to determine why something is a problem I'll consider an extreme circumstance. The question we're answering here is why cable length is an issue for digital transmission. We could, and will, study the case at the specified limit for cable length but that may not reveal what happens when we exceed the limit.

Component	Value	50 ft	328 ft	3280 ft
R	51 Ω /1,000 ft	2.55 Ω	16.73 Ω	167.3 Ω
L	160 μ H/1,000 ft	8 μ H	52.48 μ H	524.8 μ H
C	13.5 nF/1,000 ft	675 pF	4.43 nF	44.3 nF
G	100 μ S/1,000 ft	5 μ S	32.8 μ S	328 μ S

My primary purpose for including this problem is to introduce more complicated circuit analysis to our discussion regarding transfer functions. The study of transmission lines is just a nice practical application. To meet the primary goal of this example I will use mesh analysis to develop the expression for the output voltage. I've labeled the two mesh currents in the schematic above to help us write the two KVL equations needed to analyze this circuit.

$$\begin{aligned} \text{KVL } \mathbf{I}_1 & (R + Z_L + Z_C)I_1 + (-Z_C)I_2 = V_{IN} \\ \text{KVL } \mathbf{I}_2 & (-Z_C)I_1 + (Z_C + 1/G)I_2 = 0 \end{aligned}$$

We can use MATLAB to solve the system of equations. Once we have a solution for I_1 and I_2 we can find the output voltage with

$$V_{OUT} = (1/G) I_2$$

and find the transfer function with

$$H(s) = \frac{V_{OUT}}{V_{IN}}$$

Next I'll use MATLAB to substitute the part values for both lengths of cable and generate the Bode plots for both cables.

```

1  %% Finding a transfer function with Mesh Analysis
2  clear all
3  close all
4  clc
5  format short eng
6
7  syms R G L C s Vin I1 I2
8  Zl=s*L;
9  Zc=inv(s*C);
10
11 eqn(1)=(R+Zl+Zc)*I1+(-Zc)*I2==Vin;
12 eqn(2)=(-Zc)*I1+(Zc+(1/G))*I2==0;
13 sol=solve(eqn,I1,I2);
14 Vout=sol.I2*(1/G);
15

```

```

16 H=Vout/Vin;% Gain is output over input
17
18 H1s=subs(H,[R G L C],[200 5e-6 8e-6 675e-12]); %50 ft values
19 H2s=subs(H,[R G L C],[267.3 32.8e-6 52.48e-6 4.43e-9]); %328 ft values
20 H3s=subs(H,[R G L C],[2673 328e-6 524.8e-6 44.3e-9]); %3280 ft values
21 pretty(vpa(simplify(H1s),3)) %Print the transfer function in the Command
    Window
22 pretty(vpa(simplify(H2s),3)) %Print the transfer function in the Command
    Window
23 pretty(vpa(simplify(H3s),3)) %Print the transfer function in the Command
    Window
24 f=logspace(0,10,1000);
25 w=2*pi*f;
26 H1=subs(H1s,s,j*w);
27 H2=subs(H2s,s,j*w);
28 H3=subs(H3s,s,j*w);
29
30 figure(1)
31 subplot(2,1,1)
32 semilogx(f,20*log10(abs(H1)), 'LineWidth',2)
33 hold on
34 semilogx(f,20*log10(abs(H2)), 'LineWidth',2)
35 semilogx(f,20*log10(abs(H3)), 'LineWidth',2)
36 grid on
37 ylabel('Gain (dB)')
38 legend('50 ft','328 ft','3280 ft')
39
40 fig=gcf;
41 set(findall(fig,'-property','FontSize'),'FontSize',18)
42
43 subplot(2,1,2)
44 semilogx(f,angle(H1)*(180/pi), 'LineWidth',2)
45 hold on
46 semilogx(f,angle(H2)*(180/pi), 'LineWidth',2)
47 semilogx(f,angle(H3)*(180/pi), 'LineWidth',2)
48 grid on
49 xlabel('Frequency (Hz)')
50 ylabel('Phase Shift (deg)')
51
52 fig=gcf;
53 set(findall(fig,'-property','FontSize'),'FontSize',18)
54
55 %% Break the signal into phasors
56
57 syms x w t T integrand
58
59 n=100;
60 A=2.5;
61 T0=1/20e3;
62 w0=(2*pi)/T0;
63 x=@(t) A*sign(sin(w0*(t)))+A;
64 t0=0;t1=T0;
65
66 for k=0:n;
67     integrand=@(t) (x(t)).*cos(k.*w0.*t);
68     a(k+1)=(2/T0)*integral(integrand,t0,t1);

```

```

69
70     integrand=@(t) (x(t)).*sin(k.*w0.*t);
71     b(k+1)=(2/T0)*integral(integrand,t0,t1);
72 end
73
74 figure(2)
75 hold on;grid on
76 semilogy(0:length(a)-1,a,'x','LineWidth',4,'MarkerSize',10)
77 semilogy(0:length(a)-1,b,'ro','LineWidth',4,'MarkerSize',10)
78
79 xlabel('Multiple of the fundamental frequency - k')
80 ylabel('Coefficient')
81 legend('a_k','b_k')
82
83 tk=0:T0/1000:2*T0;
84 x_hat=(a(1)/2);
85 for k=1:n;
86     x_hat=x_hat+ a(k+1).*cos(k.*w0.*tk)+ b(k+1).*sin(k.*w0.*tk);
87 end
88 set(findall(gcf,'-property','FontSize'),'FontSize',14)
89
90 figure(3)
91 hold on;grid on
92 plot(tk,x(tk),'ro-','LineWidth',3)
93 plot(tk,x_hat,'LineWidth',3)
94 xlabel('Time (s)')
95 legend('x(t)','x_hat(t)')
96 set(findall(gcf,'-property','FontSize'),'FontSize',14)
97
98
99 %%
100 %DC component output
101 vo_hat=(a(0+1)/2)* (1); %DC input times DC gain
102
103 for k=1:n
104     H=subs(H1s,s,j*k*w0); % Find gain at multiple of w0
105     Vi=a(k+1)-j*b(k+1);
106     Vo=Vi*H;
107     vo_hat=vo_hat+eval(abs(Vo)).*cos(k.*w0.*tk+eval(angle(Vo)));
108 end
109
110 plot(tk,vo_hat,'g','LineWidth',3)
111 l1=line([(2/6)*T0,(2/6)*T0],[-1,6]);
112 l2=line([(5/6)*T0,(5/6)*T0],[-1,6]);
113 l3=line([(8/6)*T0,(8/6)*T0],[-1,6]);
114 l4=line([(11/6)*T0,(11/6)*T0],[-1,6]);
115 set([l1 l2 l3 l4],'LineStyle','--','LineWidth',2,'Color',[0 0 0])
116
117 a = text((1.8/6)*T0, 1.5,'RX Sample','Rotation',90);
118 a = text((4.8/6)*T0, 1.5,'RX Sample','Rotation',90);
119 a = text((7.8/6)*T0, 1.5,'RX Sample','Rotation',90);
120 a = text((10.8/6)*T0, 1.5,'RX Sample','Rotation',90);
121 xlabel('Time (s)')
122 legend('x(t)','x_hat(t)')
123 xlim([0,2*T0])
124 set(findall(gcf,'-property','FontSize'),'FontSize',14)

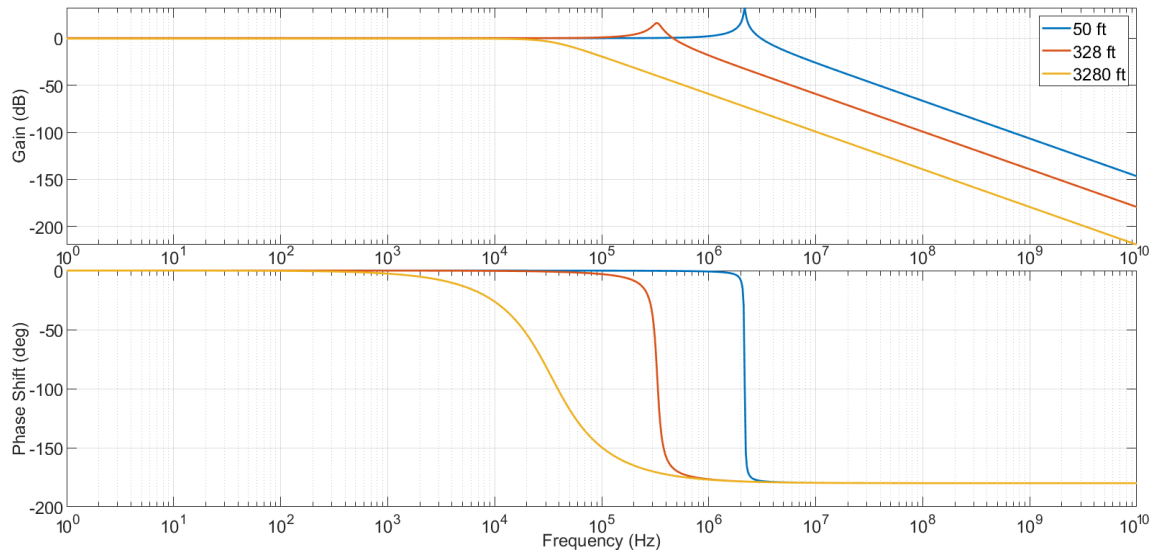
```

The transfer function for the 50 foot cable is

$$H(s) = \frac{V_{OUT}}{V_{IN}} = \frac{1}{5.4e-15s^2 + 1.76e-9s + 1}$$

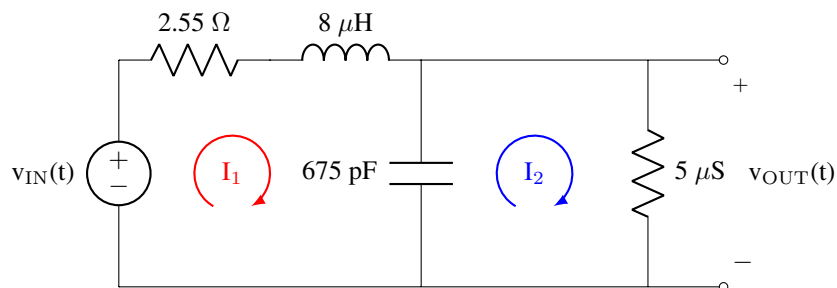
The transfer function for the 328 foot cable is

$$H(s) = \frac{V_{OUT}}{V_{IN}} = \frac{1}{232e-15s^2 + 75.8e-9s + 1}$$

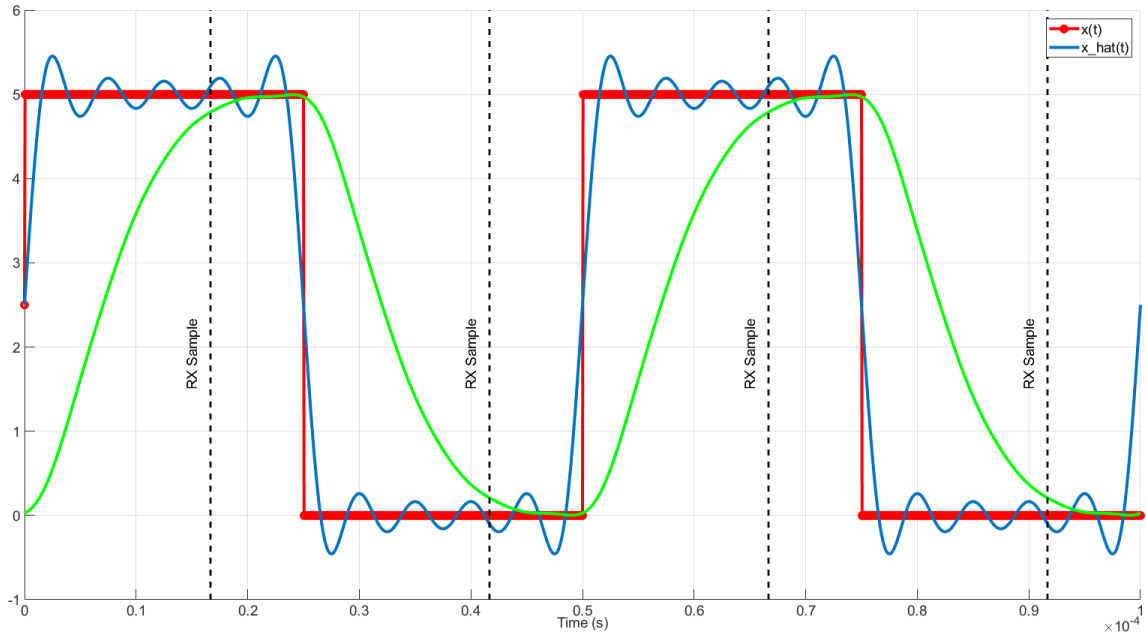
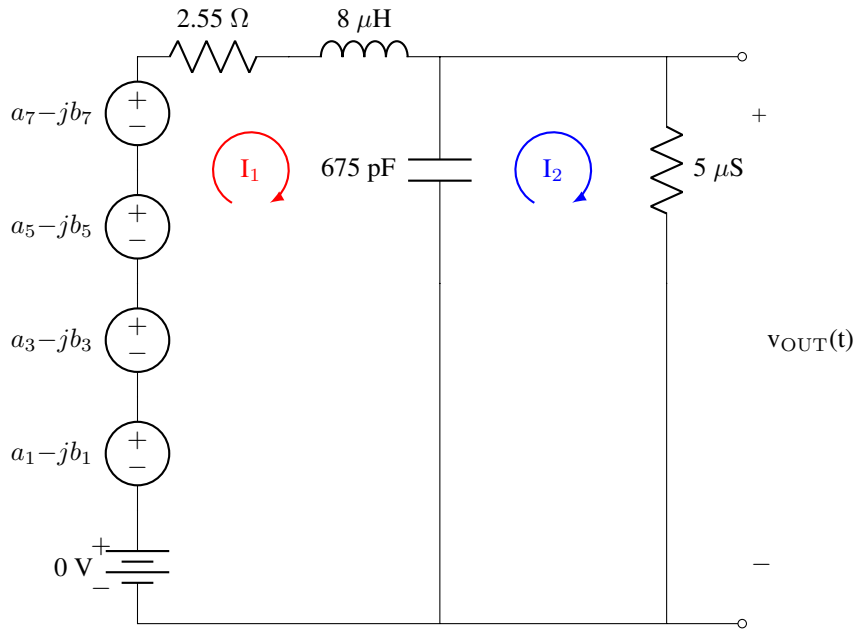


k	a _k	b _k
0	0	0
1	0	6.366
2	0	0
3	0	2.122
4	0	0
5	0	1.273
6	0	0
7	0	0.909

We can now apply the signal to the transmission line using an approximation based on the Fourier series. The voltage is applied to the transmission line as $v_{IN}(t)$ shows in the schematic below



Just as in the previous example we can break the voltage source into a source for each individual frequency. Each source, other than the DC source, will have a value of $a_k - jb_k$ using that values from the previous table. I've omitted the sources for $k = 2, 4, 6$ as they have values of 0 V. The DC source also has a value of 0 V but I included it as it is treated separately from the AC sources.



14.2 An Aperiodic Example